



# TCAD Simulation Template Setup of Novel Vertical Gallium Nitride Power Device

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## Abstract

Gallium nitride (GaN), with its wide bandgap and high critical electric field, is a key material for next-generation high-voltage, high-efficiency power devices. Vertical GaN SBDs, however, suffer from electric-field crowding at the Schottky edge when the electrode width is finite, leading to breakdown voltages far below the drift-layer limit.

This work adopts the p-GaN junction termination extension (JTE) concept in paper [1] and uses Sentaurus TCAD to compare the electric field and breakdown behavior of an ideal SBD (i-SBD), a conventional SBD (c-SBD), and a JTE-based SBD (j-SBD)

## Research Methodology

### 1. Device modeling

Built 2D vertical GaN SBDs (i-SBD, c-SBD, j-SBD) in TCAD with a common drift/substrate stack; c-SBD and j-SBD differ only in Schottky width and the presence of p-GaN JTE.

### 2. Bias and boundary conditions

Simulated forward and reverse I-V under a unified bias scheme; used an external-resistor method with  $J = 0.1 \text{ mA/cm}^2$  as the breakdown criterion.

### 3. Simulation flow

The simulation flow first sweeps drift-layer doping in i-SBD and c-SBD to establish baseline drift concentration, then introduces a p-GaN JTE and sweeps its  $n_j$ ,  $t_j$ ,  $l_j$  (Table 1), and finally extracts  $V_{BR}$ , field/impact-ionization profiles,  $R_{on,sp}$ , and BFOM.

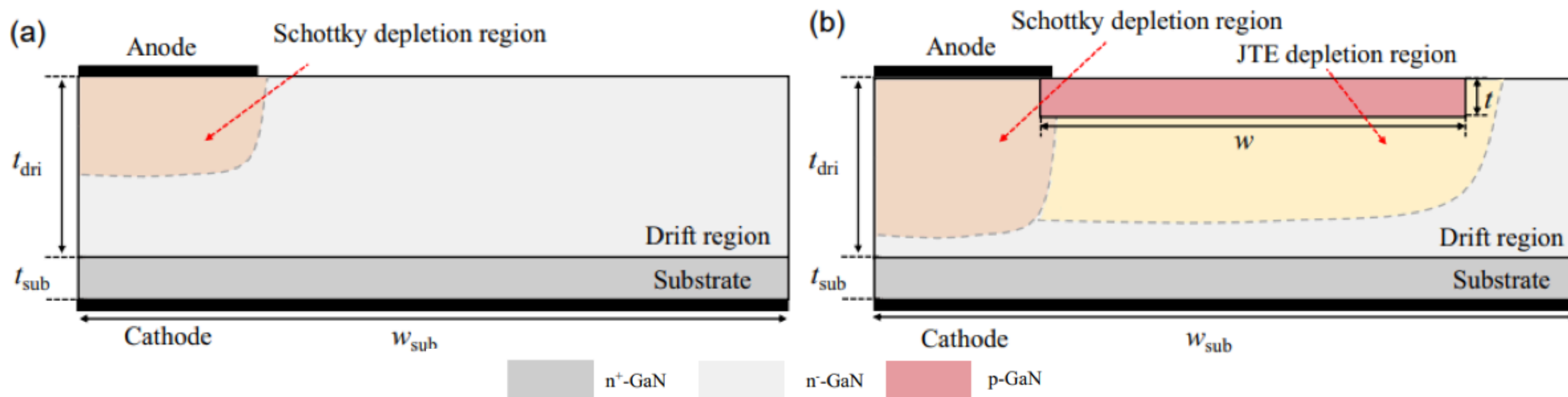


Fig 1. Schematic cross section of (a) conventional GaN SBD (C-SBD) and (b) GaN SBD with p-GaN JTE (J-SBD), reproduced from [1].

Parameter	Values
Sub $N_d$ ( $\text{cm}^{-3}$ )	$10^{18}$
Drift $N_d$ ( $\text{cm}^{-3}$ )	$10^{15}$ , $5 \times 10^{15}$ , $10^{16}$ , $5 \times 10^{16}$
JTE doping $n_j$ ( $\text{cm}^{-3}$ )	$10^{16}$ , $5 \times 10^{16}$ , $10^{17}$
JTE thickness $t_j$ ( $\mu\text{m}$ )	0.3, 0.5, 0.8
JTE length $l_j$ ( $\mu\text{m}$ )	20, 30, 40
$T_{dri}$ ( $\mu\text{m}$ )	11
$T_{sub}$ ( $\mu\text{m}$ )	2
$W_{sub}$ ( $\mu\text{m}$ )	60
$W_{cont}$ ( $\mu\text{m}$ )	10

Table 1. Key drift, JTE, and geometrical parameters used in the TCAD simulations.

## Simulation Results

(1) Edge-induced breakdown in c-SBD: With Drift  $N_d = 10^{15}$ , i-SBD reaches  $\sim 2.7 \text{ kV}$ , whereas c-SBD breaks down at only  $\sim 100 \text{ V}$  ( $\sim 3\text{-}4\%$  of the ideal value). Electric-field distribution shows a sharp peak at the Schottky edge.

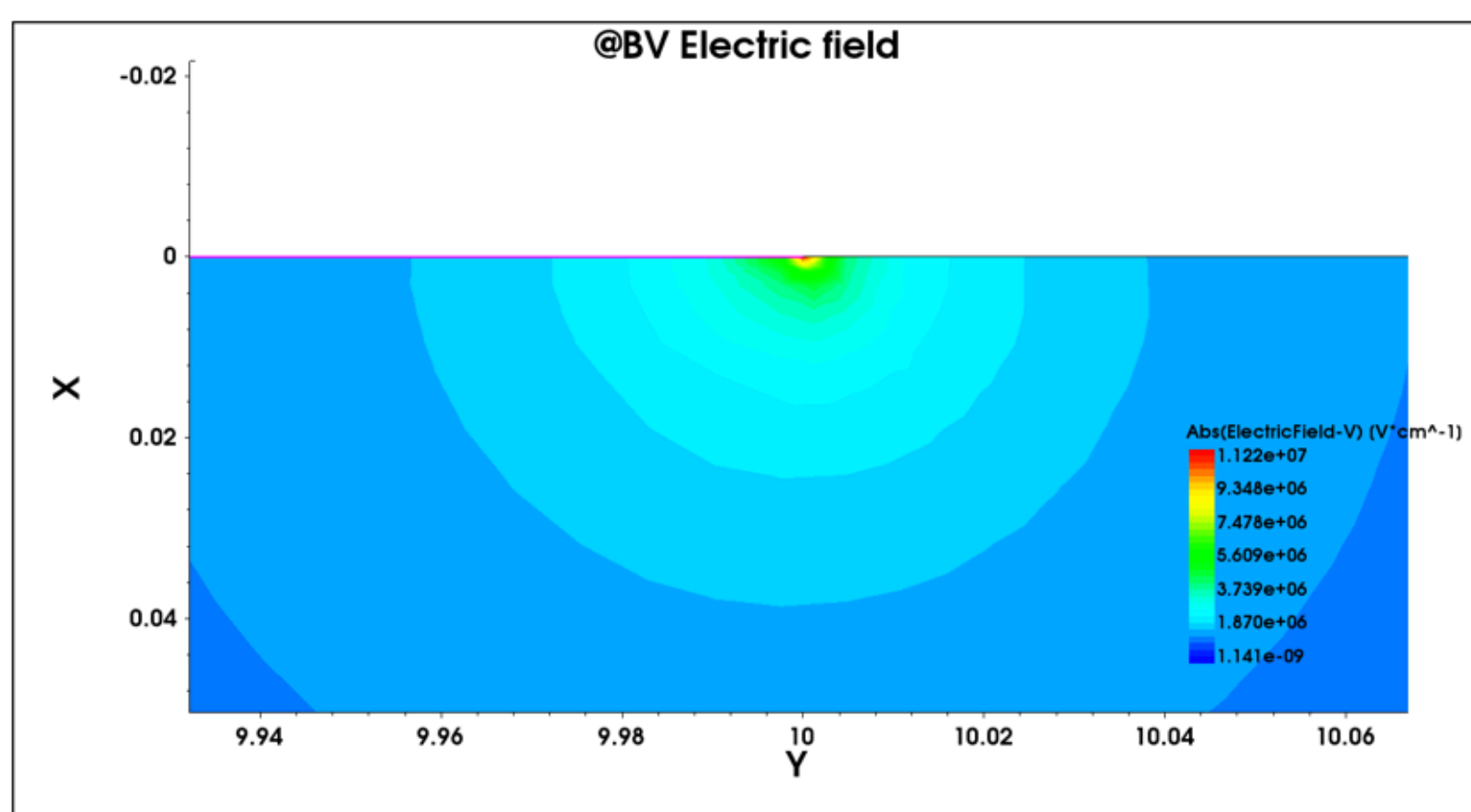


Figure 2. c-SBD electric field @BV = 103.7 V

(2) Field redistribution by j-SBD: An optimized p-GaN JTE ( $n_j \approx 1 \times 10^{17} \text{ cm}^{-3}$ ,  $t_j \approx 0.8 \mu\text{m}$ ,  $l_j \approx 40 \mu\text{m}$ ) raises BV to  $\sim 1.7 \text{ kV}$  under the same drift concentration. The peak field shifts from the metal edge into the JTE/drift region with flatter equipotential lines.

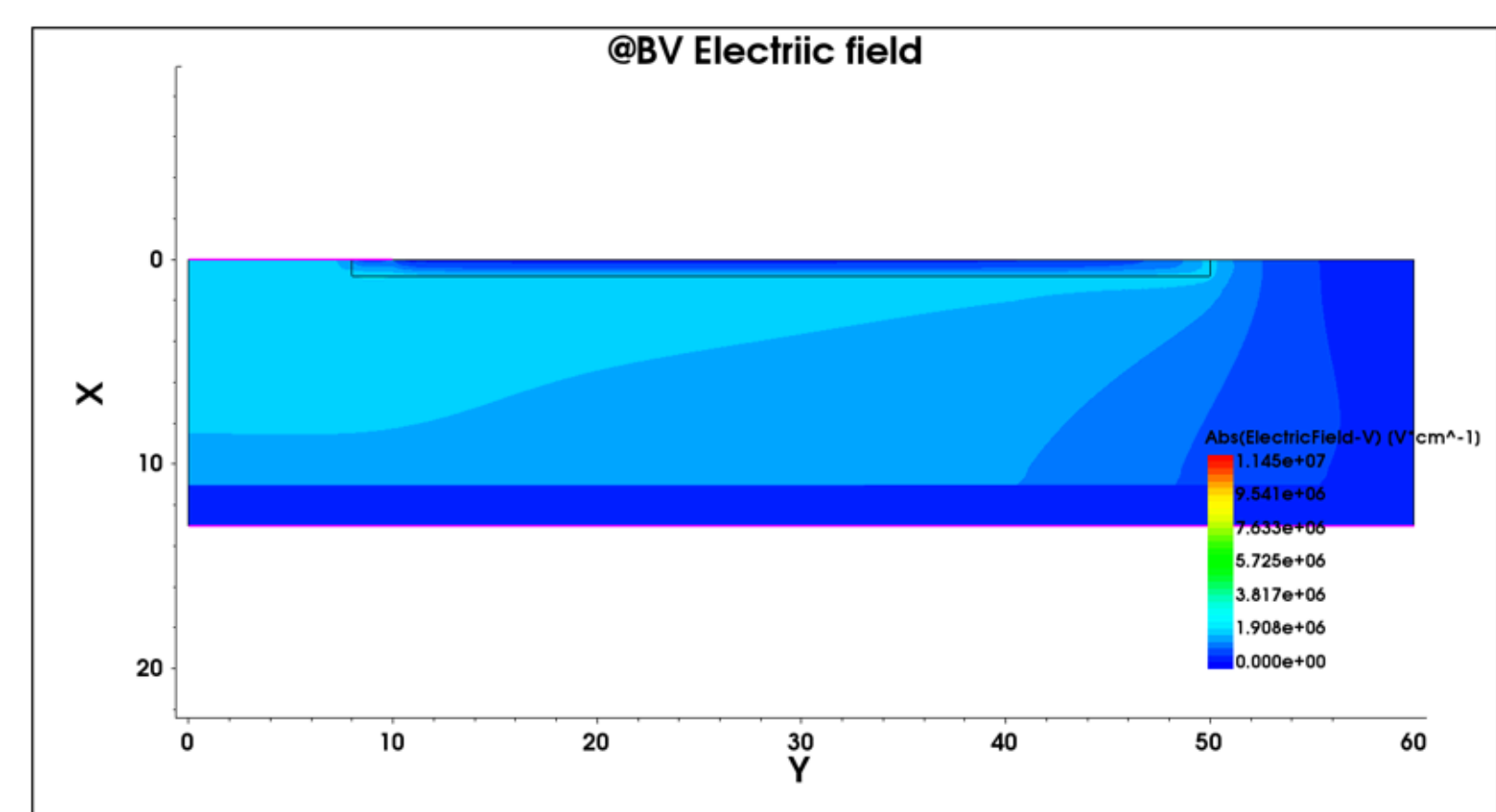


Figure 3. j-SBD electric field @BV = 1748 V

### (3) I-V characteristics comparison

Reverse bias: at  $J = 0.1 \text{ mA/cm}^2$ ,  $V_{BR} \approx 10^2 \text{ V}$  (c-SBD),  $\approx 1.7 \times 10^3 \text{ V}$  (j-SBD), and  $\approx 2.7 \times 10^3 \text{ V}$  (i-SBD).

Forward bias: all devices turn on at  $\sim 0.9 \text{ V}$ ; j-SBD has only slightly higher on-resistance, so JTE mainly enhances blocking with minor impact on conduction.

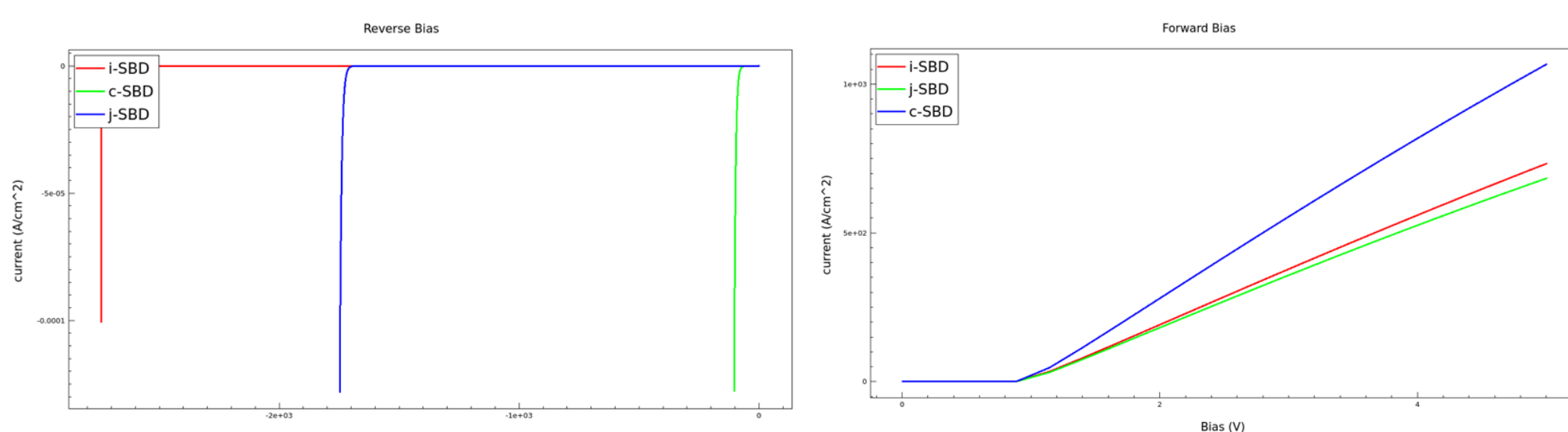


Figure 4.(a) Reverse I-V

Figure 4.(b) Forward I-V

### (4) BFOM comparison

BFOM combines  $V_{BR}$  and  $R_{on,sp}$  into a single metric to evaluate the overall power performance of a device, where a higher BFOM indicates better high-voltage, low-loss capability.

$$BFOM = \frac{V_{BR}^2}{R_{on,sp}} \propto \epsilon \mu E_c^3$$

	i-SBD	c-SBD	j-SBD
$V_{BR}$ (V)	2741	103.7	1748
$R_{on}$ ( $\text{m}\Omega \cdot \text{cm}^2$ )	5.677	3.656	5.347
BFOM ( $\text{W/cm}^2$ )	1.325G	2.941M	0.571G

Table 2. comparison of  $V_{BR}$ ,  $R_{on}$ , and BFOM